

Multiphase flow meters can be used to measure the flow rates of individual constituents within a fluid flow (e.g., a mixture of oil, gas, and water) without requiring separation of the constituents. Most of the multiphase flow meters that are currently available, however, are designed for use at the wellhead or platform. A problem with utilizing a flow meter at the wellhead of a multiple source well is that the fluid flow reaching the flow meter is a mixture of the fluids from the various sources disposed at different positions within the well. So although the multiphase meter provides the advantage of providing information specific to individual constituents within a fluid flow (which is an improvement over a bulk flow sensors), the information they provide is still limited because there is no way to distinguish sources.

Acquiring reliable, accurate fluid flow data downhole at a particular source environment is a technical challenge for at least the following reasons. First, fluid flow within a production pipe is hostile to sensors in direct contact with the fluid flow. Fluids within the production pipe can erode, corrode, wear, and otherwise compromise sensors disposed in direct contact with the fluid flow. In addition, the hole or port through which the sensor makes direct contact, or through which a cable is run, is a potential leak site. There is great advantage in preventing fluid leakage out of the production pipe. Second, the environment in most wells is harsh, characterized by extreme temperatures, pressures, and debris. Extreme temperatures can disable and limit the life of electronic components. Sensors disposed outside of the production pipe may also be subject to environmental materials such as water (fresh or salt), steam, mud, sand, etc. Third, the well environment makes it difficult and expensive to access most sensors once they have been installed and positioned downhole.

What is needed, therefore, is a reliable, accurate, and compact apparatus for sensing fluid flow within a pipe, one that can sense fluid flow within a pipe in a non-intrusive manner, one that is operable in an environment characterized by extreme temperatures and pressures and the presence of debris, one that can operate remotely, and one that is not likely to need replacement or recalibration once installed.

## DISCLOSURE OF THE INVENTION

It is, therefore, an object of the present invention to provide an apparatus for non-intrusively sensing fluid flow within a pipe that is reliable, accurate, compact, and remotely operable, one that can sense fluid flow parameters within  
5 a pipe in a non-intrusive manner, one that is operable in an environment characterized by extreme temperatures and pressures, and one that is not likely to need replacement or recalibration once installed.

According to the present invention, an apparatus for non-intrusively sensing fluid flow within a pipe is provided. The apparatus includes a first  
10 sensing array for sensing acoustic signals traveling at the speed of sound through the fluid within the pipe, a second sensing array for sensing local pressure variations traveling with the fluid flow, and a housing attached to the pipe for enclosing the sensing arrays. The first sensing array includes a plurality of first optical pressure sensors. The second sensing array includes a plurality of second  
15 optical pressure sensors.

Optical power sent from a source connected to the apparatus travels into the first sensing array, which in turn produces a first signal relating to the acoustic signals. Likewise, optical power sent from the source travels into the second sensing array, which in turn produces a second signal relating to the local  
20 pressure variations within the flow. The first and second signals are then processed and interpreted using known methods.

The function of each sensing array and the information gathered to perform that function is distinct from that of the other array, as can be clearly seen if one considers that the axial velocity of the fluid flow is small and  
25 therefore negligible compared to the speed of sound in the mixture (i.e., the speed of a compression wave traveling through the fluid within the pipe). The local pressure variations that are sensed by the second sensing array travel with the fluid flow, and are therefore at approximately the same axial velocity as the fluid flow. The local pressure variations have a small coherence length (sometimes  
30 referred to as "lengthscale") that typically lasts on the order of one to ten (1-10) pipe diameters. The acoustic signals that are sensed by the first sensing array, in contrast, are pressure variations that travel at the speed of sound through the fluid flow. The acoustic signals have a coherence length on the order of one hundred



through the cross-sectional area of the pipe. This attribute is useful for measuring propagating one-dimensional acoustic waves as well as long lengthscale vortical disturbances.

The foregoing and other objects, features and advantages of the present invention will become more apparent in light of the following detailed description of exemplary embodiments thereof.

#### BRIEF DESCRIPTION OF THE DRAWINGS

FIG.1 is a diagrammatic view of a well having a casing and a pipe, and present invention flow meters positioned at various locations along the pipe inside the casing.

FIG.2 is a diagrammatic view of an exemplary embodiment of the present invention apparatus for non-intrusively measuring fluid flow parameters within a pipe.

FIG.3 is a diagrammatic view of an embodiment of a sensing device within the present invention.

FIG.4 is a diagrammatic view of an embodiment of a sensing device within the present invention.

FIG.5 is a diagrammatic view of an embodiment of a sensing device within the present invention.

#### DETAILED DESCRIPTION OF THE INVENTION

Referring to FIG. 1 there is shown an intelligent oil well system 10 containing one or more production pipes 12 that extend downward through a casing 14 to one or more petroleum sources 16. An annulus 18 is formed between the pipe 12 and the casing 14. Each production pipe 12 may include one or more lateral sections that branch off to access different petroleum sources 16 or different areas of the same petroleum source 16. Fluid mixtures are pumped from the sources 16 to the platform 20 through the production pipes 12. The fluid mixtures consist predominantly of petroleum products and water. The production pipe 12 includes one or more the present invention apparatus 22 for non-intrusively sensing fluid flow within a pipe (also referred to hereinafter as a

“flow meter”) to monitor various physical parameters of the fluid mixtures as they flow through the production pipes 12.

The present invention flow meter 22 includes a first sensing array 24 for sensing acoustic signals traveling at the speed of sound through the fluid within the pipe 12 (hereinafter also referred to as the “SOS sensing array”), a second sensing array 26 for sensing short duration local pressure variations traveling with the fluid flow (hereinafter also referred to as the “flow velocity sensing array”), and a housing 28 attached to the pipe 12 for enclosing the sensing arrays 24,26. Each flow meter 22 can be incorporated into an existing section of production pipe 12, or can be incorporated into a specific pipe section that is inserted in line into the production pipe 12. The distributed scheme of flow meters 22 shown in FIG.1 permits an operator of the intelligent well system 10 to determine the extent and location of breakthrough of water into the petroleum reserve. The availability of this type of information permits the user to monitor and intelligently control the production of the petroleum reserve.

The sensing arrays 24,26 receive optical power and produce optical signals via fiber optic cables 30 that extend between the flow meter 22 and instrumentation (e.g., instrumentation such as, but not limited to, that disclosed in commonly assigned co-pending U.S. patent application serial no. [Docket no. CC-339], which is hereby incorporated by reference) residing on the platform 20 or at a remote location in communication with the platform 20. Optical fiber pressure sensors 32 within each sensing array 24,26 may be connected individually to the platform instrumentation, or may be multiplexed along one or more optical fibers using known techniques including, but not limited to, wavelength division multiplexing (WDM) and time division multiplexing (TDM). In those embodiments where the optical fiber pressure sensors 32 are not connected individually to the instrumentation, the sensors 32 of a sensing array 24,26 may be connected to one another in series or parallel. The optical signals produced by the sensing arrays 24,26 provide information relating to the fluid flow characteristics within the pipe 12 (e.g., local flow disturbances, acoustic wave propagation within the flow, flow pressure magnitude and changes, etc.). Interpretation of the optical signals, which can be done using methods well known in the art, enables the determination of the speed of sound (SOS) of the

fluid mixture and the velocity of the fluid flow within the pipe 12. Once the SOS, the flow velocity, the pressure, and the temperature of the mixture are known, other desirable data such as the phase fraction of the constituents within the mixture can be determined. The optical signals from the sensing arrays 24,26 may also be interpreted using the methods disclosed in the following commonly owned co-pending U.S. Patent applications, but are not limited to being used therewith: U.S. Patent application serial nos. 09/105,534 ("Fluid Parameter Measurement in Pipes Using Acoustic Pressures" filed June 26, 1998), serial no. 09/344,070 ("Measurement of Propagating Acoustic Waves in Compliant Pipes", filed 25 June 1999), serial no. 09/344,069 ("Displacement Based Pressure Sensor Measuring Unsteady Pressure in a Pipe" filed 25 June 1999), serial no. 09/344,094 ("Fluid Parameter Measurement in Pipes Using Acoustic Pressures" filed 25 June 1999), and serial no. 09/344,093 ("Non-Intrusive Fiber Optic Pressure Sensor for Measuring Unsteady Pressures within a Pipe" filed 25 June 1999), all of which are hereby incorporated by reference. FIG.2 shows an exemplary embodiment of the present invention wherein the SOS sensing array 24 and the flow velocity sensing array 26 are positioned adjacent one another on a common length of pipe 12. Further details of this embodiment are provided below. FIGS. 3-5 diagrammatically illustrate sensing array embodiments and attributes that can be used with either or both sensing arrays 24,26.

To avoid interference from outside sources and to protect from the harsh environment within the well, the sensing arrays 24,26 are enclosed within a housing 28 that is attached to an exterior surface of the pipe section 12. The housing 28 includes an outer sleeve 34 extending between a pair of bosses 36. The fiber optic cable(s) 30 that extends between the flow meter 22 and the instrumentation passes through a sealable port 38 in one or both bosses 36 and connects with the sensing arrays 24,26. Outside the housing 28, the sensor cable 30 is housed in a protective conduit 40 that is attached to the pipe 12. In the preferred embodiment, the housing 28 and the pipe 12 together form a pressure vessel. The pressure within the pressure vessel may be greater than or less than the ambient pressure within the annulus 18 between the casing 14 and the pipe 12. In other embodiments, the housing 28 is sealed to protect the sensing arrays 24,26, but does not act as a pressure vessel. In all embodiments, the size and

structure of the housing 28 are chosen to withstand the pressure gradients present in the well environment, to accommodate the size of the sensing arrays 24,26, and to allow the sensing arrays 24,26 to be positioned a distance away from the housing 28 such that heat transfer via the pipe 12 and/or the housing 28 is non-  
5    disabling for the application at hand. In a preferred embodiment, the housing 28 is filled with a gas such as, but not limited to, air, nitrogen, argon, etc. The gaseous environment within the housing 28 advantageously acts as an acoustic isolator that helps reduce pressure wave interference that might otherwise travel into the housing 28 from the annulus 18 and undesirably influence the sensing  
10    arrays 24,26. The gaseous environment also thermally insulates the sensing arrays 24,26.

In some applications, there is advantage in placing a plurality of bumpers within the housing to help maintain separation between the outer sleeve of the housing and the pipe. United States Patent Application serial number [Client  
15    Docket No. 5897-06] discloses bumpers that can be used in this manner and is hereby incorporated by reference.

The pipe section 12 has a compliancy selected to suit the application at hand. The pipe 12 must have sufficient structural integrity to handle the pressure gradient across the pipe 12, and yet must also be able to deflect (i.e., change in  
20    circumference) an amount that will yield useful information. The amount the pipe 12 will change in circumference for a given pressure distribution is determined by the thickness of the pipe wall 42 and the physical properties of the pipe material (e.g., modulus of elasticity, etc.). Thus, the thickness of the pipe wall 42 and the pipe material can be chosen to help produce a favorable sensor  
25    sensitivity for the present apparatus. The characteristics of the pipe section 12 contiguous with each present apparatus may be the same as or different than the characteristics in other sections of the production pipe 12.

The optical pressure sensors 32 used in the SOS and flow velocity sensing arrays 24,26 each include a plurality of optical fiber coils 44. Each coil 32 is  
30    wrapped one or more turns around the circumference of the pipe section 12 in a manner that allows the length of the optical fiber within the coil 32 to change in response to a change in the circumference of the pipe 12. If, for example, a pipe 12 can be expected to see a maximum circumferential change of "y", then a one-

turn coil will be subject to a maximum potential change in length of "y" (or some known function of "y"). If an optical measurement technique is not sensitive enough to register a change in distance equal to "y", then the coil 32 can be wrapped to include "n" number of turns. The change in fiber length "y" per turn is therefore multiplied by "n" turns, and a change in fiber length great enough to produce a useful signal (i.e., " $n \cdot y$ ") is provided. In fact, the same technique can be used to not only provide a minimum useful signal, but also to increase the sensitivity of the sensor 32 and therefore the range of detectable changes in the circumference of the pipe 12. In all cases, the length of the optical fiber in each coil 32 is known and is chosen to produce the sensitivity required to sense the disturbance(s) of interest for that particular sensor.. The preferred embodiment, as described above, includes coils 32 wrapped around the circumference of the pipe 12. Alternatively, the optical fiber lengths can be arranged around a portion of the circumference of the pipe 12.

The turns of optical fiber in a sensor 32 are preferably laid next to one another to minimize the axial component of each turn, and thereby keep each turn to a known, constant length. Alternatively, some or all the turns of a coil 32 could be separated from adjacent turns. A coil 32 can consist of a single layer of optical fiber turns, or multiple layers of optical fiber turns depending on the application. The coil 32 of optical fiber in each sensor 32 may be attached to the pipe 12 by a variety of attachment mechanisms including, but not limited to, adhesive, glue, epoxy, or tape. In a preferred embodiment, a tape having an adhesive substance attached to opposite surfaces of a substrate is used. The tape adheres to both the pipe 12 and the fiber and provides a smooth surface on which the fiber can be laid. It is our experience that tape used on a rough surface helps to decrease micro-bend losses within the optical fiber.

In most embodiments, the optical pressure sensors 32 used in the SOS and flow velocity sensing arrays 24,26 further include one or more optical reflective devices 46 disposed between coils 32 that are wavelength tunable. In a preferred embodiment, the optical reflective devices 46 are fiber Bragg Gratings (FBG's). An FBG, as is known, reflects a predetermined wavelength band of light having a central peak reflection wavelength ( $\lambda_b$ ), and passes the remaining wavelengths of the incident light (within a predetermined wavelength range). Accordingly, input





tunable fiber laser, examples of which can be found in U.S. Patent Nos. 5,317,576; 5,513,913; and 5,564,832, which are incorporated herein by reference.

Referring to FIG.5, in an alternative embodiment the sensors 32 may also be formed as a purely interferometric sensing array by using sensors 32 without  
5 FBG's 46 disposed therebetween. In this embodiment, each sensor 32 is independently connected to the instrumentation at the platform 20 and known interferometric techniques are used to determine the length or change in length of the fiber around the pipe 12 due to pressure variations. U.S. Patent 5,218,197,  
10 entitled "Method and Apparatus for the Non-invasive Measurement of Pressure Inside Pipes Using a Fiber Optic Interferometer Sensor", issued to Carroll discloses such a technique. The interferometric wraps may also be multiplexed in a manner similar to that described in Dandridge, et al, "Fiber Optic Sensors for Navy Applications", IEEE, Feb. 1991, or Dandridge, et al, "Multiplexed Interferometric Fiber Sensor Arrays", SPIE, Vol. 1586, 1991, pp.176-183. Other  
15 techniques to determine the change in fiber length may also be used. In addition, reference optical coils (not shown) may be used for certain interferometric approaches and may also be located on or around the pipe 12 but may be designed to be insensitive to pressure variations.

Adjacent sensors 32, within either sensing array 24,26, are spaced apart  
20 from each another by a known distance or distances. The sensors 32 in an array are preferably equidistant from one another, but not necessarily. In both sensing arrays 24,26, the spacing between adjacent sensors 32 and the number of sensors 32 reflect the nature of the signal being sensed; i.e., the SOS sensing array 24 utilizes acoustic signals having relatively long wavelengths, and the flow velocity  
25 sensing array 26 utilizes local pressure variations within the flow having relatively small coherence length. In relative terms, the sensors 32 in the SOS sensing array 24 are spaced apart from one another substantially further than are the sensors 32 within the flow velocity sensing array 26 because of the intrinsic differences in the signals being sensed. The exact inter-spacing and number of  
30 coils 32 in a sensing array 24,26 is application dependent and is a function of parameters such as, but not limited to, the spectra of anticipated acoustic signals and local pressure variations, the anticipated SOS of the fluid constituents, the number of sensors 32, the processing technique used, etc. Examples of signal

processing techniques can be found in the following references, which are incorporated herein by reference: H. Krim, M. Viberg, "Two Decades of Array Signal Processing Research - The Parametric Approach", IEEE Signal Processing Magazine, pp.67-94, R. Nielson, "Sonar Signal Processing", Ch. 2, pp.51-59.

5           FIG.2 shows an exemplary embodiment of the present invention flow meter 22 that can be inserted in-line within a production pipe 12 and disposed at an appropriate position within the well. The flow meter 22 includes a SOS sensing array 24 and a flow velocity sensing array 26 mounted on a section of pipe 12 adjacent one another and enclosed within a housing 28. A fiber optic  
10   cable 30 extends through one of the housing bosses 36 and connects to an optical delay line 48. An optical fiber 50, in turn, connects the optical delay line 48 to the SOS sensing device 24. The SOS sensing device 24 includes six (6) sensors 32 located at six predetermined locations ( $x_1, x_2, x_3, x_4, x_5, x_6$ ) along the pipe 12, where each sensor 32 is separated from adjacent sensors 32 within the SOS  
15   sensing array 24 by an axial length increment equal to " $\Delta x$ ". Each sensor is mounted on a tape that includes adhesive on both faces. A FBG 46 is positioned between the optical delay line 48 and a sensor 32. One FBG 46 is also positioned between and connected to each pair of adjacent sensors 32, such that the optical delay line 48, the FBG's 46, and the sensors 32 in the SOS sensing array 24 are in  
20   series with one another. It is preferred, but not required, to skew each FBG 46 between the adjacent sensors 32 to as to minimize the sharpness of the directional changes within the fiber of either sensor 32 or within the FBG 46.

          An optical fiber 52 extends from the last sensor 32 in the SOS sensing array 24 over to a first sensor 32 in the adjacent flow velocity sensing array 26.  
25   A FBG 46 is disposed in-line between the two devices. The flow velocity sensing array 46 includes four (4) sensors 32 located at predetermined locations ( $x_7, x_8, x_9, x_{10}$ ) along the pipe 12. Like the SOS sensing array 24, each sensor 32 in the flow velocity sensing array 26 is mounted on tape and is separated from adjacent sensor 32 within the flow velocity sensing array 26 by an axial length  
30   increment equal to " $\Delta x$ ". The axial distance  $\Delta x$  separating the sensors 32 in the flow velocity sensing array 26 is, however, substantially shorter than that used in the SOS sensing array 24 because of the difference in the characteristics of the pressure disturbances sought to be measured; i.e., the SOS sensing array 24

senses relatively long wavelength acoustic signals traveling through the fluid flow at the speed of sound, and the flow velocity sensing array 25 senses relatively short coherence length local pressure variations with the fluid flow. One FBG 46 is positioned between and connected to each pair of adjacent sensors 32, such that the FBG's 46 and the sensors 32 in the flow velocity sensing array 26 are in series with one another. Here again, it is preferred to skew each FBG 46 between the adjacent sensors 32 so as to minimize the sharp changes within the fiber of either sensor 32 or within the FBG 46. In some applications, it may be useful to connect an additional optical delay line 48 after the last sensor 32 within the flow velocity sensing array 26.

In a version of the exemplary embodiment of the present invention flow meter 22 shown in FIG.2, the optical delay line(s) 48 are formed by wrapping approximately two hundred and ten meters (210m) of optical fiber around the circumference of a three and one-half inch (3.5") diameter pipe. Each coil of the SOS sensing device 24 is formed by wrapping one hundred and two meters (102m) of optical fiber around the circumference of the pipe in a single layer. The optical fiber is wrapped using approximately twenty-five grams (25g) of tension on the fiber. Each turn of the coil is separated from adjacent coils by a fifteen micron (15 $\mu$ ) gap. Adjacent coils in the SOS sensing device are spaced approximately eighteen inches (18") apart, center to center. The velocity sensing device is formed in like manner, except that each coil comprises seven layers rather than a single layer, and adjacent coils are spaced approximately one and eight tenths of an inch (1.8") apart, center to center. In both sensing devices, the FBG's are spliced in the section of optical fiber that extends in a helical fashion between adjacent coils, or between a coil and a delay line, etc. Each FBG and the splices that tie the FBG into the optical fiber are laid on an isolator pad.

Although the invention has been described and illustrated with respect to exemplary embodiments thereof, the foregoing and various other additions and omissions may be made therein and thereto without departing from the spirit and scope of the present invention. For example, the present apparatus has been described in the Detailed Description section as being mounted on a cylindrical pipe 12. The present apparatus is not limited to cylindrical conduits, and can be used with conduits having alternative cross-sectional geometries. The Detailed

